Output-based Adaptive Methods for Large-Scale Aerodynamics Simulations

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Introduction

- Output-Based Methods
- A Steady State Result
- Unsteady Extension
- 6 A Neat Alternative





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6 Summary

The computer is not always right



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Sleipner Platform A Failure (1991)



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Discretization errors are important

Summary of AIAA DPW results (Ceze 2013)



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Uniform refinement can be misleading



DPW III wing-alone case: $M_{\infty} = 0.76$, $Re = 5 \times 10^6$. Same code but two different initial meshes (Mavriplis, 2007).

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Some definitions

Consider flow over an airfoil:



The lift adjoint Ψ_i is the sensitivity of lift to residual sources in cell *i*.

We have a solution \mathbf{U} when $\mathbf{R} = \mathbf{0}$





The lift adjoint Ψ_i is the sensitivity of lift to residual sources in cell *i*.



What if we add a residual source, $\delta \mathbf{R}_i$?



The lift adjoint Ψ_i is the sensitivity of lift to residual sources in cell *i*.



The lift adjoint Ψ_i is the sensitivity of lift to residual sources in cell *i*.



Sample steady adjoint solution



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Sample unsteady adjoint solution

Two pitching+plunging airfoils in low-Re flow

Output = lift on aft airfoil near end of simulation

Where do the residuals come from?

- A finer mesh or higher order discretization can uncover residuals in a converged solution
- Example from DG FEM:



Zero as expected

 $p_{H} = 1$

Where do the residuals come from?

- A finer mesh or higher order discretization can uncover residuals in a converged solution
- Example from DG FEM:



Nonzero: new info

 $p_h = 2$

The adjoint-weighted residual

Fine space residual, $\mathbf{R}_h(\mathbf{U}_h^H)$



Fine space adjoint, Ψ_h



Error indicator, $\epsilon_i = |\mathbf{\Psi}_{h,i}^T \mathbf{R}_{h,i} (\mathbf{U}_h^H)|$



Output error: $\delta J \approx -\Psi_h^T \mathbf{R}_h$

Idea: adapt where ϵ_i is high, to reduce residual there.

Meshing and adaptation strategies





Metric-based anisotropic mesh regeneration (e.g. BAMG software)

Riemannian ellipse







Edge Swap Edge Split Edge Collapse
Local mesh operators, and direct optimization



Cut-cell meshes: Cartesian and simplex

Typical adaptive result



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A steady-state example

DPW III wing-alone case: $M_{\infty} = 0.76, Re = 5 \times 10^6$

- In-house DG FEM code
- Initial mesh: cubic hex elements generated by agglomeration of linear multiblock meshes (first element $y^+ \approx 1$)
- Artificial viscosity shock capturing
- Spalart-Allmaras turbulence model with negative ν̃ modification [Oliver & Allmaras]
- Drag-adaptive simulation using hp discrete choice algorithm (Ceze + Fidkowski, 2013)



Contours of $\mathit{c_p}$ and $\widetilde{\nu}$

DPW wing: adapted meshes



Mach/mesh using non-zero entries cost

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DPW wing: comparison to uniform refinement



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DPW wing: comparison to uniform refinement



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Summary

- The adjoint becomes more expensive
- Adaptation is trickier need to measure space-time anisotropy



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Adaptive process for unsteady problems



Three-dimensional flapping

We apply the adaptive strategy to a three-dimensional flapping simulation.

Flow parameters

 $\textit{Re} = 500, ~~\textit{M}_{\textit{inf}} = 0.3, ~~\textit{Str} = 0.4, ~~\textit{A}_{\textit{stroke}} = \pm 30\,^{\circ}, ~~\textit{A}_{\textit{pitch}} = \pm 10\,^{\circ}$

Case parameters

- Farfield at 20+ chords
- DG1 time scheme
- The order *p* is kept between 0 and 5

• *f*_{growth} = 30%

•
$$f_{coarsen} = 5\%$$



Output: Lift integrated over final 5% of simulation time.

Adapted spatial meshes

Orders (0 to 3) plotted on entropy isosurfaces for two snapshots of the flow.



Output convergence versus DOF



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Output convergence versus CPU time



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A "free" adjoint

- An adjoint implementation is not trivial
- But we often do have a "free" adjoint: the entropy variables
 - For U = entropy function, $\mathbf{v} = U_{\mathbf{u}}$ is the entropy variable vector
 - The state v satisfies an adjoint equation!
 - The corresponding output is





• The adjoint-weighted residual becomes the entropy residual

Adapting on the entropy residual

h-Refinement on a rectangular wing in subsonic inviscid flow:



Trailing vortex in a mesh adapted on the entropy adjoint

Convergence of drag compared to output adjoints

But we lack an error estimate for an engineering output ... or do we?

We can predict drag error!

• Under a few assumptions (e.g. 2D), the approximate Oswatitsch formula gives drag:

$$D_{\rm osw} \approx \frac{u_{\infty}}{\gamma R M_{\infty}^2} \left| \int_{\mathcal{S}_{\infty}} \Delta s \, \rho \, \vec{V} \cdot \vec{n} \, dS \right|$$

- Thermodynamically equivalent to near and far-field measures
- Numerically, values will differ since flow is approximated
- Example: turbulent flow over an RAE airfoil ($Re = 6 \times 10^6$)



Initial mesh: 1610 elements

Mach number contours

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Adapting on the Oswatitsch formula



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Summary

- Output-based methods can improve efficiency and robustness of CFD in aerospace applications
- Adaptation provides tailored meshes for simulations of practical interest
- Error estimation and adaptation extend to unsteady systems
- Our methods allow us to refine space and time meshes separately by gleaning anisotropy from the error indicator
- For sufficiently-fine error tolerances, output-based adaptation saves CPU time
- "Almost" output-based methods, e.g. entropy adjoint, offer cheaper alternatives for a variety of situations

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